(12)/TR/m/25/

Appendix J:

Urban, D.L., Yuan, Z.-G., Sunderland, P.B., Lin, K.-C., Dai, Z. and Faeth, G.M. (2000) "Smoke-Point Properties of Nonbuoyant Round Laminar Jet Diffusion Flames," *Proc. Combust. Inst.* 28, 1965-1972.

Proceedings of the Combustion Institute, Volume 28, 2000/pp. 1965-1972

SMOKE-POINT PROPERTIES OF NON-BUOYANT ROUND LAMINAR JET DIFFUSION FLAMES

D. L. URBAN, ¹ Z.-G. YUAN, ¹ P. B. SUNDERLAND, ¹ K.-C. LIN, ² Z. DAI² AND G. M. FAETH²

¹NASA Glenn Research Center

Cleveland, OH 44135, USA

²University of Michigan

Ann Arbor, MI 48109, USA

The laminar smoke-point properties of non-buoyant round laminar jet diffusion flames were studied emphasizing results from long-duration (100-230 s) experiments at microgravity carried out in orbit aboard the space shuttle Columbia. Experimental conditions included ethylene- and propane-fueled flames burning in still air at an ambient temperature of 300 K, pressures of 35-130 kPa, jet exit diameters of 1.6 and 2.7 mm, jet exit velocities of 170-690 mm/s, jet exit Reynolds numbers of 46-172, characteristic flame residence times of 40-302 ms, and luminous flame lengths of 15-63 mm. Contrary to the normal-gravity laminar smoke point, in microgravity, the onset of laminar smoke-point conditions involved two flame configurations: closed-tip flames with soot emissions along the flame axis and open-tip flames with soot emissions from an annular ring about the flame axis. Open-tip flames were observed at large characteristic flame residence times with the onset of soot emissions associated with radiative quenching near the flame tip: nevertheless, unified correlations of laminar smoke-point properties were obtained that included both flame configurations. Flame lengths at laminar smoke-point conditions were well correlated in terms of a corrected fuel flow rate suggested by a simplified analysis of flame shape. The present steady and nonbuoyant flames emitted soot more readily than non-buoyant flames in earlier tests using ground-based microgravity facilities and than buoyant flames at normal gravity, as a result of reduced effects of unsteadiness, flame disturbances, and buoyant motion. For example, present measurements of laminar smokepoint flame lengths at comparable conditions were up to 2.3 times shorter than ground-based microgravity measurements and up to 6.4 times shorter than buoyant flame measurements. Finally, present laminar smoke-point flame lengths were roughly inversely proportional to pressure to a degree that is a somewhat smaller than observed during earlier tests both at microgravity (using ground-based facilities) and at normal gravity.

Introduction

The laminar smoke-point properties of jet diffusion flames (the luminous flame length, fuel flow rate, characteristic residence time, etc., at the onset of soot emissions) are useful observable soot properties of non-premixed flames. For example, these measures provide a means to rate several aspects of flame sooting properties: the relative propensity of various fuels to produce soot in flames [1-4]; the relative effects of fuel structure, fuel dilution, flame temperature, and ambient pressure on the soot emission properties of flames [5-14]; the relative levels of continuum radiation from soot in flames [15–17]; and effects of the intrusion of gravity (buoyancy) on emissions of soot from flames [18-26]. Laminar smoke-point properties generally are measured using buoyant round laminar jet diffusion flames, surrounded by co-flowing air in order to prevent pulsations characteristic of buoyant jet diffusion flames in still environments. Laminar smoke-point properties found using this configuration are relatively independent of burner diameter and co-flow

velocities, which tends to enhance their value as global measures of soot properties [9,10]. Recent studies, however, suggest that the laminar smoke-point properties of buoyant and non-buoyant laminar jet diffusion flames are fundamentally different [19–26]. Thus, the overall objective of the present investigation was to measure the laminar smoke-point properties of non-buoyant flames, because of the relevance of non-buoyant flames to most practical industrial processes where effects of buoyancy are small.

The potential differences between the laminar smoke properties of buoyant and non-buoyant flames can be attributed mainly to the different hydrodynamic properties of these flames [24–27]. In particular, soot particles are too large to diffuse like gas molecules so that they are convected at gas velocities, aside from minor effects of Brownian motion and thermophoresis [24]. In non-buoyant flames, the streamlines diverge from the nozzle axis, whereas in buoyant flames the streamlines (and the entrained flow) converge toward the nozzle axis. As

a result, flow acceleration due to gravitational forces in buoyant round laminar jet diffusion flames implies that soot mainly nucleates near the flame sheet and then is drawn toward fuel-rich conditions nearer to the flame axis, promoting soot growth for an extended residence time before the soot finally crosses the flame sheet within an annular soot layer near the flame tip to reach soot oxidation conditions. This type of soot path, termed soot-formation flame conditions by Kang et al. [27], tends to promote soot growth and inhibit soot oxidation, enhancing the tendency of the flame to emit soot. On the other hand, flow deceleration in non-buoyant round laminar jet diffusion flames implies that soot mainly nucleates in the cool core of the flame at fuel-rich conditions and then is drawn directly toward and through the flame sheet, so that soot tends to leave the flame over a relatively extended region. This type of soot path, termed soot-formation-oxidation conditions by Kang et al. [27], tends to inhibit soot growth and enhance soot oxidation compared to buoyant flames that have similar characteristic residence times, reducing the tendency of the flame to emit soot. Thus, the soot nucleation, growth, and oxidation environments of buoyant and non-buoyant laminar jet diffusion flames are quite different, providing significant potential for different laminar smoke-point properties

Several studies of the laminar smoke-point properties of non-buoyant laminar jet diffusion flames have been reported, motivated by the potential effects of buoyancy on soot processes in flames (see Refs. [18-25] and references cited therein). Most of these studies used ground-based microgravity facilities to observe non-buoyant flames and showed that laminar smoke-point flame lengths were significantly smaller and laminar smoke-point characteristic residence times were significantly larger for non-buoyant than buoyant flames. These differences generally have been attributed to the different soot paths in buoyant and non-buoyant flames that were just discussed, as well as increased effects of radiative quenching in non-buoyant flames due to their increased characteristic residence times compared to buoyant flames. A concern about these results, however, is that limited testing using space-based microgravity facilities yielded significantly different results than those observed using ground-based microgravity facilities [25]. Thus, the objective of the present study was to more completely assess these differences by measuring laminar smoke-point properties during long-term experiments (100-230 s) at microgravity carried out on orbit in the space shuttle Columbia (flights STS-83 and STS-94 in 1997). The scope of the study was limited to round ethyleneand propane-fueled laminar jet diffusion flames burning in still and slightly vitiated air at pressures of 35-130 kPa.

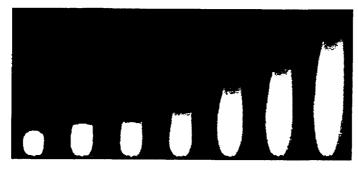
Experimental Methods

Experimental methods are described only briefly, see Urban et al. [25] for details about the apparatus and instrumentation and Lin et al. [28] for a tabulation of test conditions. The laminar jet diffusion flames were stabilized at the exit of round fuel nozzles located along the axis of a windowed chamber having a diameter and length of 400 mm and 740 mm, respectively. The chamber was filled with oxygen/nitrogen mixtures to provide the nominal composition of dry air (21 \pm 1% oxygen by volume). The properties of the gas surrounding the flames varied slightly over the present relatively long test times because the test chamber was closed. The greatest change involved the gas composition, but even this change was modest, with maximum oxygen consumptions never exceeding 0.02 mol fraction during any test. These conditions were maintained by periodically venting the chamber to space and adding fresh dry air in the period between tests. Present flames typically required 10 s times to approach steady behavior as exemplified by constant flame lengths after a disturbance [25].

Stainless steel fuel nozzles having inside diameters of 1.6 mm and 2.7 mm, lengths of 148 mm, and inlet flow straighteners yielded nonswirling fully developed laminar flow at the jet exit. The test fuels were stored in cylinders and delivered to the nozzles through solenoid valves and a mass flow rate controller and sensor. The flames were ignited with a hot wire coil that was retracted from the nozzle exit once the flame was stabilized.

Monitoring measurements included the fuel flow rate, the fuel inlet temperature, the chamber pressure, and the chamber gas temperature [25,28]. The flames were observed using a color CCD video camera (Hitachi, Model KP-C553) with a 125 × 164 mm field of view and a 25 mm depth of field centered on the flame axis. Flame images were recorded at a rate of 30 images/s and could be measured with a spatial resolution better than 0.3 mm. Initial fuel flow rates were set in excess of laminar smoke-point flow rates and could be adjusted up to $\pm 30\%$ in 5% steps to achieve the desired final conditions near (within 5%), but generally smaller than, laminar smoke-point fuel flow rates. Three tests were exceptions in which initial excessively large fuel flow rates prevented final flame lengths from being shorter than laminar smoke-point conditions, as noted by Lin et al. [28].

A total of 21 flames were observed, yielding the following ranges of test properties: ethylene- and propane-fueled flames, ambient air temperatures and pressures of 300 K and 35–130 kPa, respectively, jet exit velocities and Reynolds numbers of 170–1690 mm/s and 46–172, respectively, characteristic residence times of 40–302 ms, and luminous flame lengths of 15–63 mm. Characteristic residence times



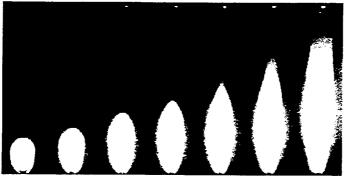


Fig. 1. Photographs of round nonbuoyant laminar jet diffusion flames in still air as the fuel flow rate is increased in the transition region where the laminar smoke-point is approached and exceeded for ethylenefueled flames with a 1.6 mm jet exit diameter. Upper series of photographs shows open-tip smoke-point behavior at 100 kPa, with the third flame from the left just beyond the smoke-point condition; lower series of photographs shows closed-tip smoke-point behavior at 50 kPa, with the fifth flame from the left just beyond the smoke-point condition.

are reported elsewhere [29] and are taken to be $2L/u_0$.

Results and Discussion

Flow Visualization

Typical of many past observations of non-buoyant round laminar jet diffusion flames [18-22,24,25,28], the present flames could be grouped into closed-tip and open-tip configurations. The difference between these two configurations was particularly noticeable in the vicinity of the laminar smoke-point, as illustrated by the images in Fig. 1. These photographs show the flame appearance as the fuel flow rate is increased in the transition region where the laminar smoke-point is approached and exceeded for ethylene-fueled flames having 1.6 mm jet exit diameters. The upper series of photographs shows the behavior of large characteristic residence time flames (larger than 80 ms) where the flame tips were blunt (opentip) throughout the transition to soot emitting conditions, and the first emission of soot was associated with an annular region surrounding the flame axis and having a diameter comparable to the maximum flame diameter. The lower series of photographs shows the behavior of small characteristic residence time flames (smaller than 80 ms) where the flame tips were rounded (closed-tip) and the first emission of soot was along the flame axis. Even these latter flames, however, eventually exhibited open-tip behavior as fuel flow rates increased beyond the laminar smoke-point condition (see the last image of the lower series of photographs in Fig. 1). Thus, tip opening generally is closely associated with laminar smoke-point conditions for non-buoyant flames, which has also been observed by several other investigators (see Refs. [18–22] and references cited therein).

Measurements of soot concentrations in the present flames using deconvoluted laser extinction show that soot is contained within a narrow annular ring and that no soot is present at the flame axis for open-tip conditions [25]. Corresponding soot temperatures using deconvoluted multiline emission measurements show that soot temperatures progressively decrease with increasing streamwise distances in open-tip flames and reach values of roughly 1000 K near the flame tip [25]. Low reaction rates at such conditions are consistent with quenching of soot oxidation, allowing soot to escape from the flame. The main mechanism causing this progressive reduction of temperature is continuum radiation from soot. This radiative heat loss becomes more significant with increasing streamwise distance due to the progressive reduction of flow velocities, which involves a corresponding reduction of transport and thus reaction rates at the flame sheet. The corresponding reduced chemical energy release rates, combined with progressively increasing radiative heat losses due to increasing soot concentrations,

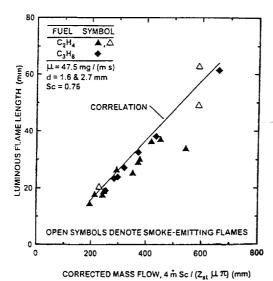


Fig. 2. Luminous flame lengths as a function of corrected fuel flow rate for round non-buoyant laminar jet diffusion flames in still air at the laminar smoke point. Correlation based on simplified analysis of Lin et al. [28].

provide ample potential for quenching, and thus tipopening, and corresponding emissions of soot. In contrast, buoyant diffusion flames have progressively increasing velocities and thus increasing transport rates with increasing streamwise distance, due to effects of buoyancy, so that soot emissions occur because of rapid mixing and residence times that are insufficient to complete soot oxidation, rather than because of radiative quenching [25]. Finally, this latter condition is approached by non-buoyant flames at short residence times where effects of radiative quenching are reduced, which tends to produce the closed-tip laminar smoke-point behavior illustrated in the lower series of photographs of Fig. 1.

Luminous Flame Lengths

Similar to the observations of luminous flame lengths at the smoke-points of buoyant round laminar jet diffusion flames as described by Schug et al. [5], the present luminous flame lengths at the smoke points of non-buoyant round laminar jet diffusion flames were closely associated with the fuel flow rate, as suggested by the simplified analysis of Lin et al. [28]. This behavior is illustrated in Fig. 2, where present measurements of laminar smoke-point luminous flame lengths are plotted as a function of the corrected fuel flow rate based on the results of the simplified flame shape theory for non-buoyant laminar jet diffusion flames of Ref. [28]. The open symbols on this plot denote the three test conditions in which soot-emitting flames just beyond the laminar

smoke-point conditions were measured; nevertheless, these measurements are very similar to the remaining results which are from flames at the laminar smoke point but which were not emitting soot. The one data point remote from the rest resulted at at the lowest pressure tested, 35 kPa, at which luminous flame lengths and the onset of soot-emitting conditions were more difficult to observe due to relatively small maximum soot concentrations (less than I ppm based on multiline emission measurements). Except for the one outlier, the correlation between luminous flame lengths and corrected fuel mass flow rates at laminar smoke-point conditions is seen to be quite good; therefore, laminar smokepoint properties will be represented by luminous flame lengths alone to simplify the comparison between present measurements and the earlier findings in Refs. [5,16,24].

An explanation of the luminous flame length behavior observed in Fig. 2 can be obtained from the flame shape correlations of Lin et al. [28] for nonbuoyant round laminar jet diffusion flames in still air. These results are based on a simplified analysis (Spalding [29]) for this flame configuration. Ignoring small effects of the virtual origin, this correlation can be written to yield the luminous flame length as a function of the corrected fuel flow rate parameter used in Fig. 2, as follows:

$$L = (3C_f/32)(4\dot{m} \ Sc/(Z_{\rm st} \ \mu\pi)) \tag{1}$$

where the empirical parameter Cf is used to account for the presence or absence of soot within the flame. Following Ref. [28], a simple correlation of equation I was fitted to the measurements of flames in air environments using values of Sc and μ for air at roughly the average of the adiabatic flame temperature and the ambient temperature (the values used are summarized on the plot). The correlation shown in the figure is for $C_{\rm f}=1$ for flames at the laminar smoke point from Lin et al. [28], in contrast to $C_{\rm f}$ = 0.5 for soot-free blue flames from Sunderland et al. [30]. The longer soot-containing flames are consistent with luminosity due to the presence of soot at fuel-lean conditions for flames at the transition to soot emissions [28]. Finally, it is evident that equation I provides a surprisingly good correlation between luminous flame lengths and the corrected mass flow rate for present observations of non-buoyant round laminar jet diffusion flames in spite of the approximate nature of the Spalding [29] analysis.

Laminar Smoke Points

In view of the different mechanisms leading to the onset of soot emissions for buoyant and non-buoyant laminar jet diffusion flames, it is not surprising that they have substantially different laminar smokepoint properties. This behavior is illustrated in Figs. 3 and 4 by plots of laminar smoke-point flame

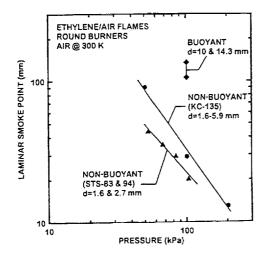


Fig. 3. Laminar smoke-point flame lengths of ethylenefueled round non-buoyant and buoyant laminar jet diffusion flames burning in air as a function of pressure. Nonbuoyant KC-135 results from Sunderland et al. [24], buoyant results from Schug et al. [5] and Sivathanu and Faeth [16].

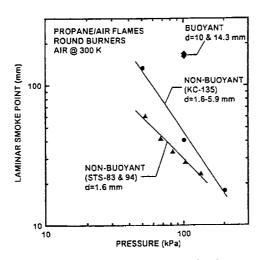


FIG. 4. Laminar smoke-point flame lengths of propanefueled round non-buoyant and buoyant laminar jet diffusion flames burning in air as a function of pressure. Nonbuoyant KC-135 results from Sunderland et al. [24], buoyant results from Schug et al. [5] and Sivathanu and Faeth [16].

lengths as a function of pressure for ethylene- and propane-fueled flames. Measurements illustrated in the figures include results for non-buoyant flames having jet exit diameters of 1.6 and 2.7 mm from the present space-based experiments, results for non-buoyant flames having jet exit diameters of 1.6, 2.7 and 5.6 mm from Sunderland et al. [24] using

ground-based microgravity facilities, and results for buoyant flames having jet exit diameters of 10.0 mm from Schug et al. [5] and 14.3 mm from Sivathanu and Faeth [16].

There are several interesting features about the measurements illustrated in Figs. 3 and 4. First of all, an obvious feature of these results is that the present laminar smoke-point flame lengths of the non-buoyant flames are significantly smaller than those of the buoyant flames. For example, the laminar smoke-point flame lengths of the buoyant flames are up to 6.4 times larger than the present non-buoyant flames at comparable conditions. This behavior comes about because the present nonbuoyant flames have much larger characteristic residence times (up to 300 ms [28]) than the buoyant flames (only up to 50 ms [24]), which is due to buoyancy-induced motion, in spite of the greater length of the buoyant flames. This provides greater potential for radiative heat losses for the non-buoyant flames, leading to the radiative quenching mechanism of soot emissions discussed in connection with tip openings (Fig. 1).

Another important feature of the laminar smokepoint flame lengths illustrated in Figs. 3 and 4 is that the present non-buoyant flames are significantly smaller than those of nonbuoyant flames in groundbased microgravity facilities (which typically have gravity of 10^{-2} g) up to a factor of 2.3 at comparable conditions. This behavior is caused by the closer approach to steady, non-buoyant flame properties by the long-term space-based experiments compared to the relatively unsteady and disturbed microgravity environment of ground-based microgravity facilities. Flow velocities are very small near the flame tip of non-buoyant laminar jet diffusion flames [24] and can be disturbed by small levels of g-jitter resulting enhanced mixing, which defers radiative quenching. This behavior is exacerbated by the relatively slow development of non-buoyant flames for the relatively large jet exit diameters considered during the ground-based microgravity tests, so flame response times were generally longer than periods when the test apparatus was free of disturbances [25]. Further evidence of enhanced mixing in the ground-based microgravity tests compared to the space-based tests is provided by the observations of generally shorter luminous flame lengths at comparable conditions for the ground-based results (e.g., 30% shorter as discussed by Lin et al. [28]).

Another difference between the laminar smokepoint properties of non-buoyant flames from ground- and space-based microgravity facilities involves the pressure dependence. In particular, the present long-term microgravity experiments yield laminar smoke-point flame lengths that are roughly inversely proportional to pressure. This effect of pressure comes about because increased pressures tend to increase rates of soot formation [11–14], and because of residence times available for soot growth for given burner conditions and flame lengths: both these effects imply smaller flame lengths for onset of soot emissions as pressures increase. In contrast, the more disturbed microgravity environment of the ground-based facilities yields laminar smoke-point flame lengths that are inversely proportional to pressure to the 1.4 power. This latter behavior is a stronger pressure variation than that observed for buoyant flames. Flower and Bowman [11-14] report laminar smoke-point flame lengths inversely proportional to pressure to the 1.3 power. These variations of the pressure dependence of laminar smoke-point flame lengths due to the intrusion of disturbances and gravitational forces are not surprising, however, because flame response to these effects varies with pressure. Differences of these magnitudes are of interest for gaining a better understanding of soot formation in diffusion flames (see Glassman [10]), which highlights the importance of achieving truly steady and non-buoyant diffusion flame conditions for reliable experimental results.

Other properties of the laminar smoke-point flame lengths plotted in Figs. 3 and 4 are qualitatively similar for non-buoyant space-based flames, non-buoyant ground-based flames, and buoyant flames. For example, effects of jet exit diameter on laminar smoke-point flame lengths are small in all three cases, which agrees with the well-known behavior of buoyant flames (see Glassman [9,10]). This behavior is expected for buoyant flames because their flame heights and characteristic residence times are both independent of jet exit diameter, with the latter being largely a function of flame height [16]. This behavior is not expected for non-buoyant flames, however, because while their flame lengths are independent of jet exit diameter, as discussed in connection with Fig. 2, their characteristic residence times decrease with decreasing jet exit diameter [24], which should contribute to corresponding increases of laminar smoke-point flame lengths. Such increases are not observed, and this behavior merits further study. Finally, the laminar smoke-point flame lengths of ethylene-fueled flames are smaller than those of propane-fueled flames for all three flame conditions considered in Figs. 3 and 4. This behavior agrees with past observations of the greater propensity to soot of ethylene-fueled compared to propanefueled laminar jet diffusion flames [5,15,16].

Conclusions

The smoke-point properties of nonbuoyant round laminar jet diffusion flames were observed during long-term (100-230 s) experiments at microgravity using space-based facilities. Measurements included ethylene- and propane-fueled flames burning in still air at an ambient temperature of 300 K, pressures

of 35-130 kPa, jet exit diameters of 1.6 and 2.7 mm, jet exit velocities of 170-1690 mm/s, jet exit Reynolds numbers of 46-172, characteristic flame residence times of 40-302 ms, and luminous flame lengths of 15-63 mm. The major conclusions of the study are as follows:

1. The onset of laminar smoke-point conditions in microgravity involved either a closed-tip configuration with first soot emissions along the flame axis, or an open-tip configuration with first soot emissions from an annular ring about the flame axis and having a diameter comparable to the maximum flame diameter. Closed- and open-tip flames were observed at small and large characteristic flame residence times, respectively, supporting earlier observations that open-tip behavior is caused by radiative quenching of soot oxidation near the flame tip

2. Luminous flame lengths at laminar smoke-point conditions were equally well correlated for both closed- and open-tipped flame configurations in terms of a corrected fuel flow rate, independent of the jet exit diameter, as suggested by the simplified flame shape analysis of Lin et al. [28]. These laminar smoke-point flame lengths were roughly 30% longer than those measured using ground-based microgravity facilities because of decreased effects of unsteadiness and g-jitter.

3. The present steady and non-buoyant flames emitted soot more readily than other non-buoyant flames at microgravity in ground-based facilities and than buoyant flames at normal gravity. For example, the laminar smoke-point flame lengths of non-buoyant flames from ground-based micro-gravity facilities were up to 2.3 times longer than the present measurements at comparable conditions because of effects of unsteadiness and g-jitter; similarly, the laminar smoke-point flame lengths of buoyant flames were up to 6.4 times longer than the present measurements at comparable conditions because of effects of buoy-

ancy-induced motion.

4. Laminar smoke-point flame lengths as a function of pressure were identical for both closed- and open-tipped flames and were roughly inversely proportional to pressure and relatively independent of jet exit diameter for the present nonbuoyant flames. In contrast, the laminar smokepoint flame lengths of non-buoyant flames in ground-based microgravity facilities and buoyant flames at normal gravity were inversely proportional to pressure to the 1.4 and 1.3 powers, respectively, because of effects of unsteadiness, g-jitter, and buoyancy-induced motion. All flame conditions considered, however, indicated that laminar smoke-point flame lengths are generally smaller for ethylene than for propane, reflecting the greater propensity to soot of ethylene compared to propane.

Nomenclature

- C_f flame length parameter
- d fuel port diameter
- D mass diffusivity
- L laminar smoke-point flame length
- m fuel mass flow rate
- p pressure
- Re flame Reynolds number, $4 \dot{m}/(\pi d\mu)$
- Re_o jet exit Reynolds number, $4 m/(\pi d\mu_o)$
- Sc Schmidt number, v/D
- u streamwise velocity
- Z_{st} stoichiometric mixture fraction
- μ dynamic viscosity
- ν kinematic viscosity
- ρ density

Subscript

burner exit condition

Acknowledgments

This research was supported by NASA Grants NCC3-661, NAG3-1878, and NAG3-2048 of the Office of Life and Microgravity Sciences under the overall technical management of H. D. Ross of the Glenn Research Center. The authors acknowledge the efforts R. Crouch, G. T. Linteris, and J. E. Voss, who actually carried out the experiments in orbit, and A. Over and her associates at the Glenn Research Center for development and operation of the test apparatus.

REFERENCES

- Clarke, A. E., Hunter, T. C., and Garner, F. H., J. Inst. Petrol. 32:627-642 (1946).
- Schalla, R. L., Clark, T. P., and McDonald, G. E., NACA report 1186, 1954.
- Schalla, R. L., and McDonald, G. E., Proc. Combust. Inst. 5:316–324 (1954).
- 4. Schalla, R. L., and Hubbard, R. R., NACA report 1300,
- Schug, K. P., Manheimer-Timnat, Y., Yaccarino, P., and Glassman, I., Combust. Sci. Technol. 22:235-250 (1080)
- Glassman, I., and Yaccarino, P., Proc. Combust. Inst. 18:1175-1183 (1980).

- Glassman, I., and Yaccarino, P., Combust. Sci. Technol. 24:107-114 (1980).
- Gomez, A., Sidebotham, G., and Glassman, I., Combust. Flame 58:45-57 (1984).
- 9. Glassman, I., Proc. Combust. Inst. 22:295-311 (1988).
- Glassman, I., Proc. Combust. Inst. 27:1589–1596 (1998).
- Flower, W. L., and Bowman, C. T., Combust. Sci. Technol. 37:93-97 (1984).
- Flower, W. L., and Bowman, C.T., Proc. Combust. Inst. 20:1035-1044 (1984).
- Flower, W. L., and Bowman, C. T., Proc. Combust. Inst. 21:1115-1129 (1986).
- Flower, W. L., and Bowman, C. T., Combust. Sci. Technol. 53:217-224 (1987).
- Markstein, G. H., Proc. Combust. Inst. 22:363–370 (1988)
- Sivathanu, Y. R., and Faeth, G. M., Combust. Flame 81:133-149 (1990).
- Köylü, Ü. Ö., and Faeth, G. M., Combust. Flame 87:61-76 (1991).
- Ito, H., Fujita, A., and Ito, K., Combust. Flame 99:363–370 (1994).
- Ku, J. C., Griffin, D. W., Greenberg, P. S., and Roma, J., Combust. Flame 102:216-218 (1995).
- Megaridis, C. M., Griffin, D. W., and Konsur, K., Proc. Combust. Inst. 26:1291–1299 (1996).
- Konsur, B., Megaridis, C. M., and Griffin, D. W., Combust. Flame 116:334-347 (1998).
- Konsur, B., Megaridis, C. M., and Griffin, D. W., Combust. Flame 118:509-520 (1999).
- Atreya, A., and Agrawal, S., Combust. Flame 115:372

 382 (1998).
- Sunderland, P. B., Mortazavi, S., Faeth, G. M., and Urban, D. L., Combust. Flame 96:97-103 (1994).
- Urban, D. L., Yuan, Z.-G., Sunderland, P. B., Linteris,
 G. T., Voss, J. E., Lin, K.-C., Dai, Z., Sun, K., and
 Faeth, G. M., AIAA J. 36:1346-1360 (1998).
- Law, C. K., and Faeth, G. M., Prog. Energy Combust. Sci. 20:65-113 (1994).
- Kang, K. T., Hwang, J. Y., Chung, S. M., and Lee, W., Combust. Flame 109:266-281 (1997).
- Lin, K.-C., Faeth, G. M., Sunderland, P. B., Urban, D. L., and Yuan, Z.-G., Combust. Flame 116:415-431
- Spalding, D. B., Combustion and Mass Transfer, Pergamon Press, New York, 1979, pp. 185-195.
- Sunderland, P. B., Mendelson, B. J., Yuan, Z.-G., and Urban, D. L., Combust. Flame 116:376-386 (1999).

COMMENTS

John L. de Ris, Factory Mutual Research, USA. Your instrumentation includes a radiometer. One wonders whether the total radiative fraction from the flame at its smoke point at zero-gravity takes on the same value of 30% as is found for normal buoyant flames at their smoke-point. For normal buoyant flames, this radiant fraction is independent of fuel type. You also measured the flame tip temperature of flames at their smoke-point condition. How does this temperature compare to the 1400 K value found for smoke-point flames for normal gravity?

Author's Reply. The total radiative fraction from the flames we studied was between 40% and 60%. Since most of our flames were very near the smoke height, the limited data set studied here did not show evidence of a correlation between radiative emission and smoke height as reported for normal-gravity flames.

As reported (Ref. [25] in paper), the extrapolated temperatures (from the multiline emission measurements) at the flame tip (at the smoke point) were approximately 1000 K. This is substantially lower than the 1400 K value reported by other workers for normal-gravity flames.

Fletcher J. Miller, National Center for Microgravity Research, USA. Since the laminar smoke points are so dependent on residence time, how might the presence of a co-flow in the 1g experiments versus the absence of a co-flow in the µg experiments affect the comparison between the two gravitational levels? Would µg experiments with a co-flow be valuable to provide an independent way to alter residence times?

Author's Reply. Co-flow flames are used in 1g smokepoint studies to eliminate buoyancy induced flicker. In 1g, the co-flow has a very limited effect on the flame residence time (and likewise on the smoke point) which are dominated by the buoyant acceleration. In low gravity, the situation is quite different: the flow diverges from the nozzle; consequently, the velocity at the flame tip can be quite small and is therefore easily influenced (increased) by the co-flow. We agree with the suggestion that testing with coflow in low gravity should provide interesting results, and this is part of a planned future experiment.